

Understanding Jacobian Algebra for my paper: 77 New Thermodynamic Identities among Crystalline Material Properties Leading to a Shear Constitutive Law in Isotropic Solids. The thermodynamics has 7 independent variables: all 6 stresses and temperature. The system is a free energy with iso-piezo mechanics. In that sense, the system is a Gibbs like free energy. What is given below can be used to evaluate any of the Jacobian tables in the *Journal of Applied Physics* paper.

Consider the following 8 equations:

$$y_1 = y_1(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_2 = y_2(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_3 = y_3(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_4 = y_4(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_5 = y_5(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_6 = y_6(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_7 = y_7(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

$$y_8 = y_8(x_1, x_2, x_3, x_4, x_5, x_6, x_7)$$

Their chain rule derivatives are

$$dy_1 = \frac{\partial y_1}{\partial x_1} dx_1 + \frac{\partial y_1}{\partial x_2} dx_2 + \dots \frac{\partial y_1}{\partial x_7} dx_7$$

$$dy_2 = \frac{\partial y_2}{\partial x_1} dx_1 + \frac{\partial y_2}{\partial x_2} dx_2 + \dots \frac{\partial y_2}{\partial x_7} dx_7$$

⋮

$$dy_8 = \frac{\partial y_8}{\partial x_1} dx_1 + \frac{\partial y_8}{\partial x_2} dx_2 + \dots \frac{\partial y_8}{\partial x_7} dx_7$$

Let y_1 and y_2 vary while holding y_3, y_4, \dots, y_8 constant. The following 8 homogeneous equations are found:

$$\begin{aligned}
0 &= -dy_1 + \frac{\partial y_1}{\partial x_1} dx_1 + \frac{\partial y_1}{\partial x_2} dx_2 + \dots \frac{\partial y_1}{\partial x_7} dx_7 \\
0 &= -dy_2 + \frac{\partial y_2}{\partial x_1} dx_1 + \frac{\partial y_2}{\partial x_2} dx_2 + \dots \frac{\partial y_2}{\partial x_7} dx_7 \\
0 &= 0 + \frac{\partial y_3}{\partial x_1} dx_1 + \frac{\partial y_3}{\partial x_2} dx_2 + \dots \frac{\partial y_3}{\partial x_7} dx_7 \\
&\vdots \\
0 &= 0 + \frac{\partial y_8}{\partial x_1} dx_1 + \frac{\partial y_8}{\partial x_2} dx_2 + \dots \frac{\partial y_8}{\partial x_7} dx_7
\end{aligned}$$

or

$$\begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} -dy_1 & \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_7} \\ -dy_2 & \frac{\partial y_2}{\partial x_1} & \frac{\partial y_2}{\partial x_2} & \dots & \frac{\partial y_2}{\partial x_7} \\ 0 & \frac{\partial y_3}{\partial x_1} & \frac{\partial y_3}{\partial x_2} & \dots & \frac{\partial y_3}{\partial x_7} \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \frac{\partial y_8}{\partial x_1} & \frac{\partial y_8}{\partial x_2} & \dots & \frac{\partial y_8}{\partial x_7} \end{pmatrix} \bullet \begin{pmatrix} 1 \\ dx_1 \\ dx_2 \\ dx_3 \\ dx_4 \\ dx_5 \\ dx_6 \\ dx_7 \end{pmatrix}$$

The determinate of the matrix must be zero for a solution

$$0 = \det \begin{vmatrix} -dy_1 & \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_7} \\ -dy_2 & \frac{\partial y_2}{\partial x_1} & \frac{\partial y_2}{\partial x_2} & \dots & \frac{\partial y_2}{\partial x_7} \\ 0 & \frac{\partial y_3}{\partial x_1} & \frac{\partial y_3}{\partial x_2} & \dots & \frac{\partial y_3}{\partial x_7} \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots \\ 0 & \frac{\partial y_8}{\partial x_1} & \frac{\partial y_8}{\partial x_2} & \dots & \frac{\partial y_8}{\partial x_7} \end{vmatrix}$$

Evaluating the determinate using Cramer's Rule gives

$$0 = -dy_1 \left(\det \begin{vmatrix} \frac{\partial y_2}{\partial x_1} & \frac{\partial y_2}{\partial x_2} & \dots & \frac{\partial y_2}{\partial x_7} \\ \frac{\partial y_3}{\partial x_1} & \frac{\partial y_3}{\partial x_2} & \dots & \frac{\partial y_3}{\partial x_7} \\ \dots & \dots & \dots & \dots \\ \frac{\partial y_8}{\partial x_1} & \frac{\partial y_8}{\partial x_2} & \dots & \frac{\partial y_8}{\partial x_7} \end{vmatrix} \right) + dy_2 \left(\det \begin{vmatrix} \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_7} \\ \frac{\partial y_3}{\partial x_1} & \frac{\partial y_3}{\partial x_2} & \dots & \frac{\partial y_3}{\partial x_7} \\ \dots & \dots & \dots & \dots \\ \frac{\partial y_8}{\partial x_1} & \frac{\partial y_8}{\partial x_2} & \dots & \frac{\partial y_8}{\partial x_7} \end{vmatrix} \right) \text{ so}$$

$$\frac{\partial y_1}{\partial y_2} \Big|_{y_3, y_4, \dots, y_8} = \frac{\det \begin{vmatrix} \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_7} \\ \frac{\partial y_3}{\partial x_1} & \frac{\partial y_3}{\partial x_2} & \dots & \frac{\partial y_3}{\partial x_7} \\ \dots & \dots & \dots & \dots \\ \frac{\partial y_8}{\partial x_1} & \frac{\partial y_8}{\partial x_2} & \dots & \frac{\partial y_8}{\partial x_7} \end{vmatrix}}{\det \begin{vmatrix} \frac{\partial y_2}{\partial x_1} & \frac{\partial y_2}{\partial x_2} & \dots & \frac{\partial y_2}{\partial x_7} \\ \frac{\partial y_3}{\partial x_1} & \frac{\partial y_3}{\partial x_2} & \dots & \frac{\partial y_3}{\partial x_7} \\ \dots & \dots & \dots & \dots \\ \frac{\partial y_8}{\partial x_1} & \frac{\partial y_8}{\partial x_2} & \dots & \frac{\partial y_8}{\partial x_7} \end{vmatrix}}$$

or

$$\frac{\partial y_1}{\partial y_2} \Big|_{y_3, y_4, \dots, y_8} = \frac{J(y_1, y_3, y_4, y_5, y_6, y_7, y_8)}{J(y_2, y_3, y_4, y_5, y_6, y_7, y_8)}$$

Tables 1-5 in the text are all written to be in Jacobian format so any partial derivative can be found. For example

$$\frac{\partial y_1}{\partial y_2} \Big|_{y_3, y_4, \dots, y_8}$$

is formed by reading the rows in the tables. MatLab works well in evaluating the 7X7 determinates. For example:

```

%% Evaluation of determinates from Jacobians in Strain Volume Thermodynamics
%% c is constant stress heat capacity; T is absolute temperature;
%% betai are crystallographic thermal expansion coefficients; v is volume
%% per unit mass; sij are elastic compliances.

```

```

syms c T v beta1 beta2 beta3 beta4 beta5 beta6 s11 s12 s13 s14 s15 s16

```

```

M1=[c/T, v*beta1, v*beta2, v*beta3, v*beta4, v*beta5, v*beta6;

```

```

    1, 0, 0, 0, 0, 0, 0;

```

```

    0, 0, 1, 0, 0, 0, 0;

```

```

    0, 0, 0, 1, 0, 0, 0;

```

```

    0, 0, 0, 0, 1, 0, 0;

```

```

    0, 0, 0, 0, 0, 1, 0;

```

```

    0, 0, 0, 0, 0, 0, 1]

```

```

det(M1)

```

```

M2= [ v*beta1, v*s11, v*s12, v*s13, v*s14, v*s15, v*s16;

```

```

    1, 0, 0, 0, 0, 0, 0;

```

```

    0, 0, 1, 0, 0, 0, 0;

```

```

    0, 0, 0, 1, 0, 0, 0;

```

```

    0, 0, 0, 0, 1, 0, 0;

```

```

    0, 0, 0, 0, 0, 1, 0;

```

```

    0, 0, 0, 0, 0, 0, 1]

```

```

det(M2)

```

```

det(M1)/det(M2)

```

Which has a MatLab evaluation as:

M1 =

```

[ c/T, beta1*v, beta2*v, beta3*v, beta4*v, beta5*v, beta6*v]

```

```

[ 1, 0, 0, 0, 0, 0, 0]

```

```

[ 0, 0, 1, 0, 0, 0, 0]

```

```

[ 0, 0, 0, 1, 0, 0, 0]

```

```

[ 0, 0, 0, 0, 1, 0, 0]

```

```

[ 0, 0, 0, 0, 0, 1, 0]

```

```

[ 0, 0, 0, 0, 0, 0, 1]

```

ans =

```

-beta1*v

```

M2 =

```

[ beta1*v, s11*v, s12*v, s13*v, s14*v, s15*v, s16*v]

```

```

[ 1, 0, 0, 0, 0, 0, 0]

```

```

[ 0, 0, 1, 0, 0, 0, 0]

```

```

[ 0, 0, 0, 1, 0, 0, 0]

```

```

[ 0, 0, 0, 0, 1, 0, 0]

```

```

[ 0, 0, 0, 0, 0, 1, 0]

```

```

[ 0, 0, 0, 0, 0, 0, 1]

```

ans =

```

-s11*v

```

ans =
beta1/s11

so the above expression used in equation (17) is evaluated as

$$\frac{\partial \epsilon}{\partial \Omega_1} \Big|_{T, \sigma_2, \dots, \sigma_6} = \frac{J(\epsilon, T, \sigma_2, \sigma_3, \sigma_4, \sigma_5, \sigma_6)}{J(\Omega_1, T, \sigma_2, \sigma_3, \sigma_4, \sigma_5, \sigma_6)} = \frac{\beta_1}{S_{11}}$$